

# FNAL to DUSEL long baseline experiment

- Milind Diwan (BNL, USA)  
7/16/2009 FNAL meeting
- Issues regarding pressure  
performance of tubes



# PMT considerations

	10 inch R7081	20 inch R3600
Number (25% cov)	~50000	~14000
QE	25%	20%
CE	~80%	~70%
rise time	4 ns	10 ns
Tube length	30 cm	68 cm
Weight	1150 gm	8000 gm
Vol.	~5 lt	~50 lt
pressure rating	0.7Mpa	0.6Mpa
* coverage/pmt	0.6 deg	1.1 deg
*granularity	1.0 deg	2.1 deg



# PMT: further choice

Items	Example 12-inch PMT	R7081 10-inch PMT	R5912 8-inch PMT
Diameter	300 mm	253 mm	202 mm
Effective Area	280 mm min.	220 mm min.	190 mm min.
Tube Length	330 mm	245 mm	220 mm
Dynodes	LF/10-stage	LF/10-stage	LF/10-stage
Applied Voltage	1500 V	1500 V	1500 V
GAIN	1.00E+07	1.00E+07	1.00E+07
T.T.S.(FWHM)	2.8 ns	2.9 ns	2.4 ns
P/V Ratio	2.5	2.5	2.5
Dark Counts	10,000 cps	7,000 cps	4,000 cps

**NEW !**

**HAMAMATSU**  
HAMAMATSU PHOTONICS K.K. Electron Tube Division



M.Diwan





R5912  
R5912-02

R7081  
R7081-20

R8055

R3600-02  
R7250



# SPECIFICATIONS

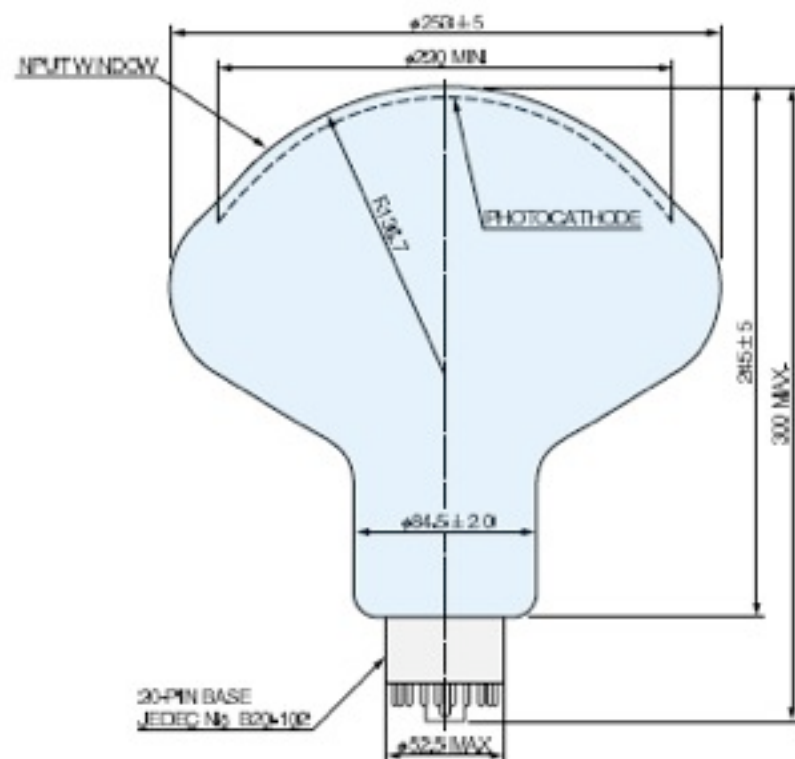
Type No.	Cathode Sensitivity						Anode Sensitivity			
	Luminous (2856 K)		Radiant at 420 nm	Blue Sensitivity Index (CS 5-58)		Quantum Efficiency at 390 nm	Luminous (2856 K)	Radiant at 420 nm	Gain	Applied Voltage for Typical Gain
	Min. (μA/lm)	Typ. (μA/lm)		Min.	Typ.					
R5912	40	70	72	6.0	9.0	22	700	$7.2 \times 10^5$	$1.0 \times 10^7$	1500
R5912-02	40	70	72	6.0	9.0	22	70 000	$7.2 \times 10^7$	$1.0 \times 10^9$	1700
R7081	40	80	80	6.0	10.0	25	800	$8.0 \times 10^5$	$1.0 \times 10^7$	1500
R7081-20	40	80	80	6.0	10.0	25	80 000	$8.0 \times 10^7$	$1.0 \times 10^9$	1700
R8055	35	60	65	5.5	8.0	20	600	$6.5 \times 10^5$	$1.0 \times 10^7$	1500
R3600-02	35	60	65	5.5	8.0	20	600	$6.5 \times 10^5$	$1.0 \times 10^7$	2000
R7250	35	60	65	5.5	8.0	20	600	$6.5 \times 10^5$	$1.0 \times 10^7$	2000

NOTE: Anode characteristics are measured with the voltage distribution ratio shown below.  
 ( ): Measured with the special voltage distribution ratio (Tapered Divider) shown below.

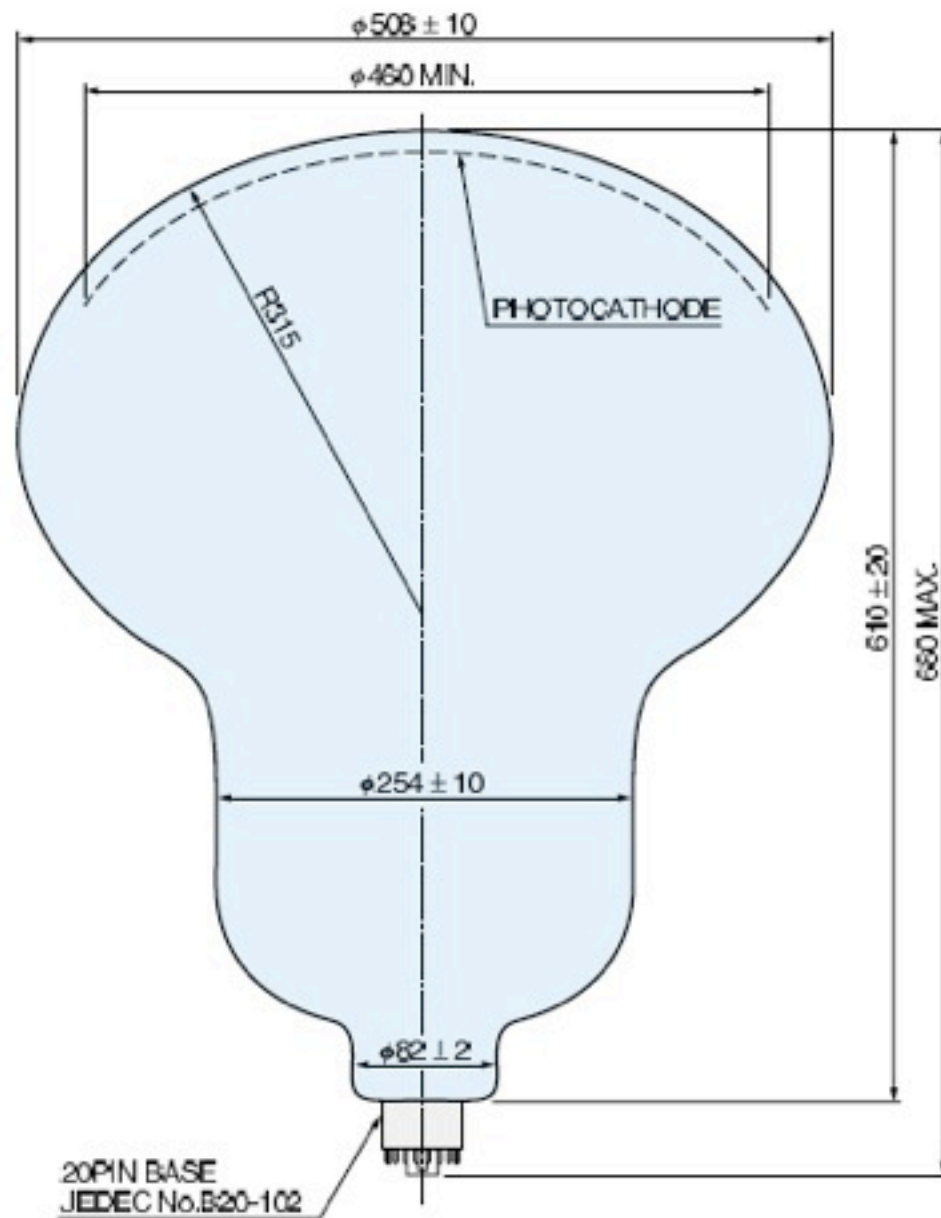
Type No.	Maximum Ratings							
	Supply Voltage		Average Anode Current	Operating Ambient Temperature	Storage Temperature	Pressure	Direct Interelectrode Capacitances	
	Anode to Cathode (V)	Anode to Last Dynode (V)					Anode to Last Dynode (pF)	Anode to All Other Dynodes (pF)
R5912	2000	300	0.1	-30 to +50	-30 to +50	0.7	approx. 3	approx. 7
R5912-02	2000	300	0.1	-30 to +50	-30 to +50	0.7	approx. 3	approx. 7
R7081	2000	300	0.1	-30 to +50	-30 to +50	0.7	approx. 3	approx. 7
R7081-20	2000	300	0.1	-30 to +50	-30 to +50	0.7	approx. 3	approx. 7
R8055	2500	300	0.1	-30 to +50	-30 to +50	0.15	approx. 10	approx. 20
R3600-02	2500	300	0.1	-30 to +50	-30 to +50	0.6	approx. 36	approx. 40
R7250	2500	300	0.1	-30 to +50	-30 to +50	0.6	approx. 10	approx. 15

We are focussed on the R7081 tube  
 It is more efficient than the R3600.  
 $25\% * R7081 \Rightarrow 35\% * R3600$

●R7081, R7081-20



●R3600-02



# Final choices and notes from meeting with vendor

- R708I - Pressure rating from manufacturer appears valid and likely conservative.
- R708I with high QE: already developed. will have same pressure rating.
- Any additional pressure resistance could be implemented, but development will cost \$. Vendor has a computer model to determine the tube pressure performance.
- 12 inch tube will likely have same pressure rating. 12 inch tube was to be available in February, but no communication so far.
- 12 inch with high QE is not in the development path currently.

# Pressure testing



Have 32 phototubes from Hamamatsu. Pressure vessel from BNL. Evolving testing protocol.

Hamamatsu rating is ~7atm. Tested this tube until it broke at 148 psi (~10atm)



# Data so far

PMT	size	Break Press
R708I/ng 1	10inch	148 psi
XPI807 1	12 inch	92 psi
xp18060 1	8 inch	35 psi
R708I 2	10 inch	cycled 132psi
R708I 3	10 inch	cycled 132 psi
R708I 4	10 inch	cycled 132 psi
R708I/lowr 1	10 inch	205 psi
R708I/lowr 2	10 inch	218 psi
R708I	10 inch	292 psi
ETL 9350ka	8 inch	68 psi
R708I	10 inch	173 psi

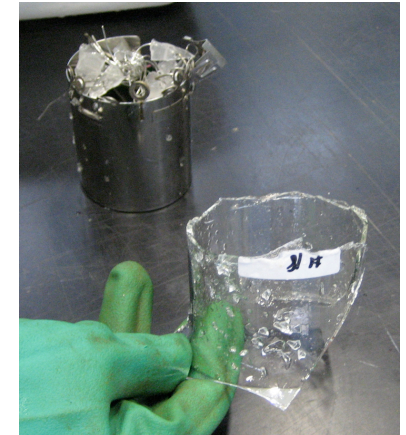
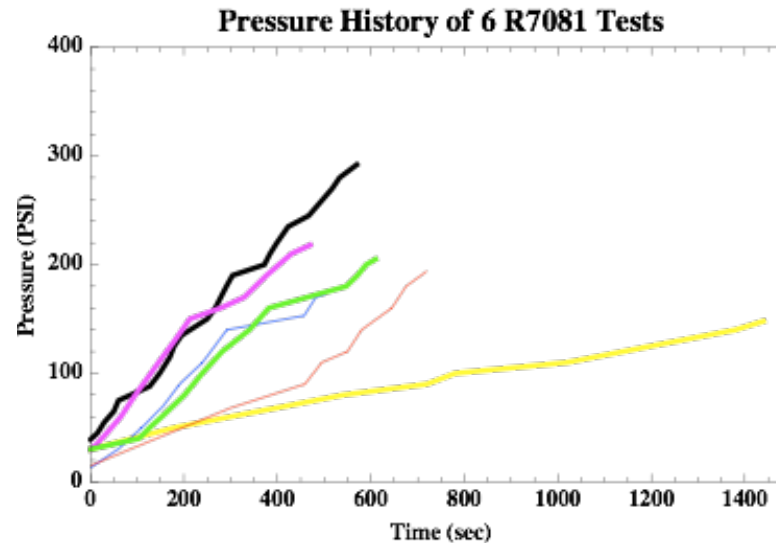
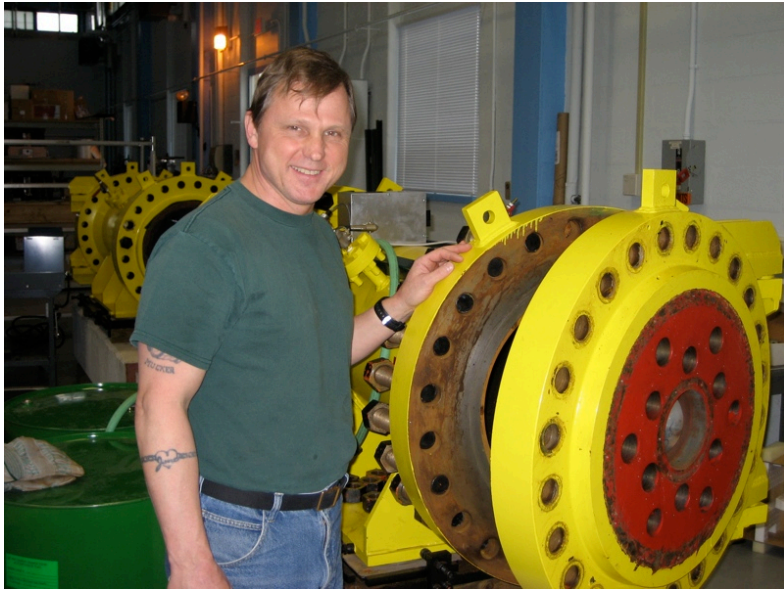
Hamamatsu tested 3 R708I upto ~10 atm.

One broke at 10 atm,

On each tube, there is data on glass thickness, pressure pulse duration, etc.

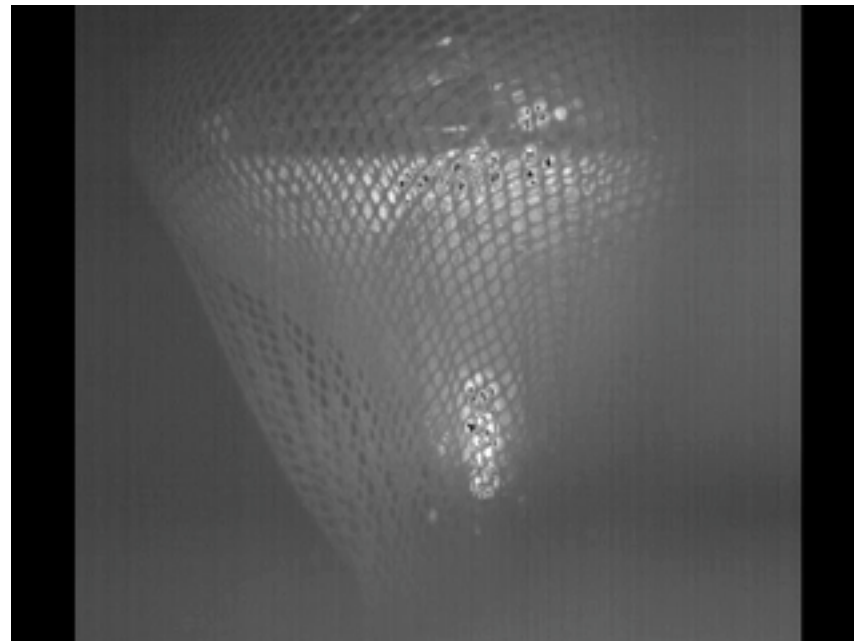
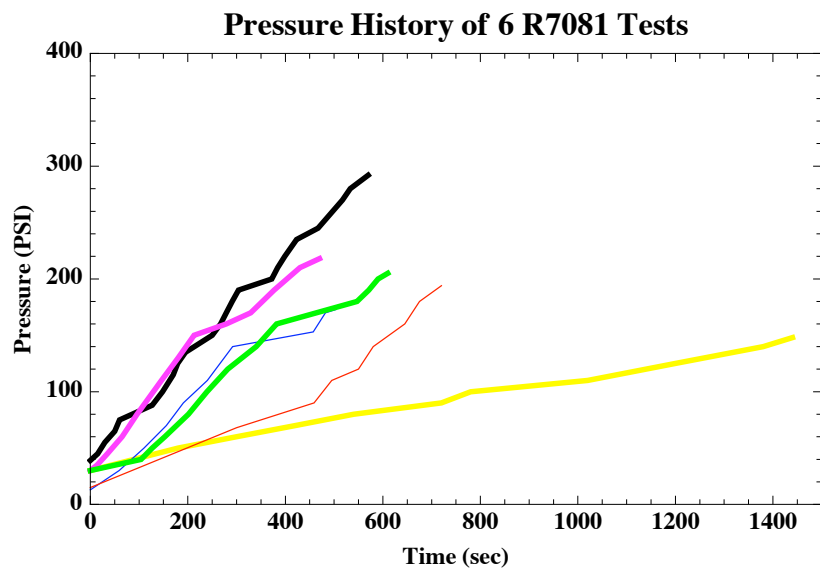
This is borosilicate glass with thickness ranging from 0.08 to 0.12 inch.

# Development of pressure testing at BNL (Diwan, Goett, Sexton)

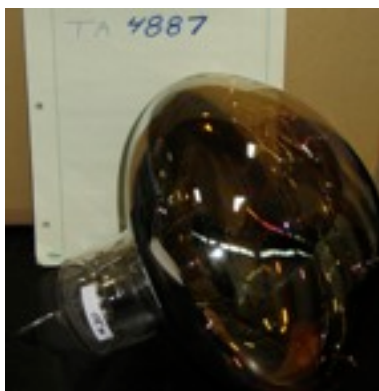


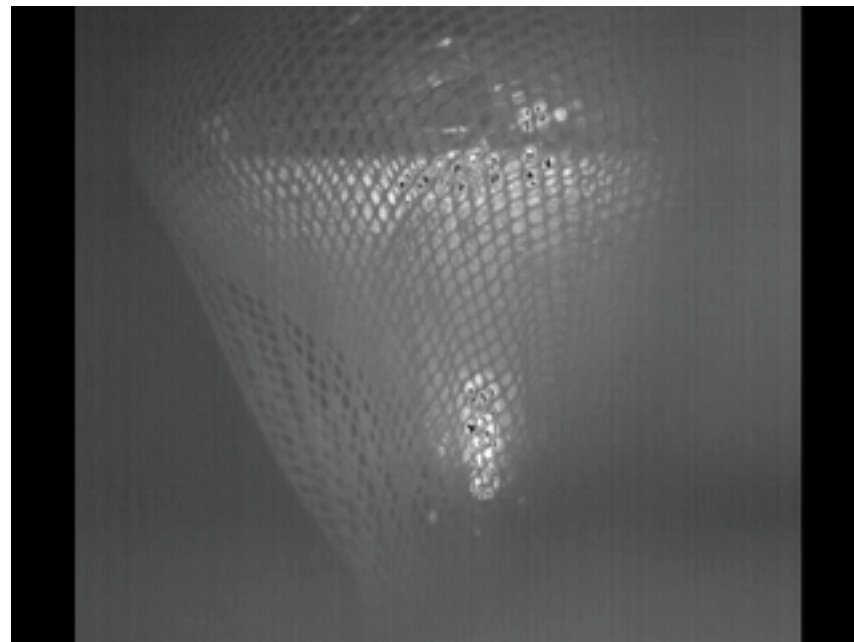
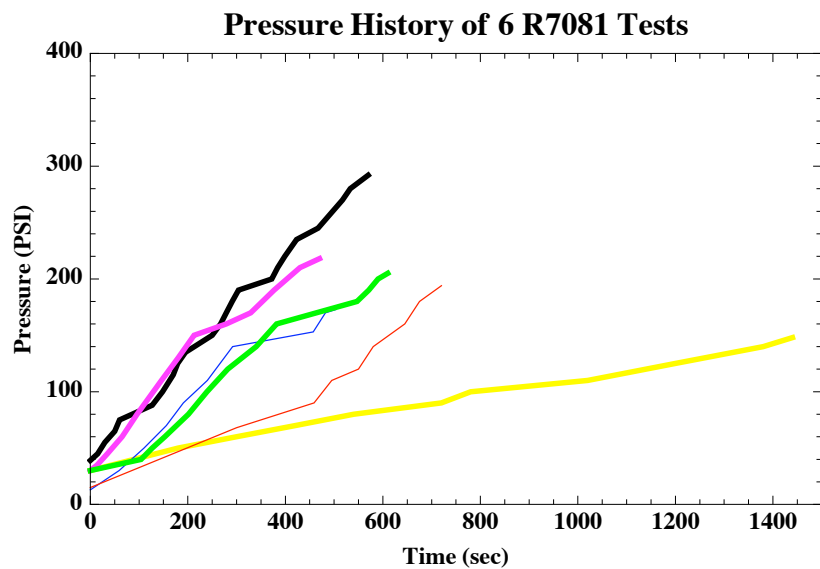
- What have we learned
  - Manufacturers have tubes with very distinct characteristics
  - Failure mode in Hamamatsu hemispherical tubes is at the pins. 7 atm is o.k.
  - Other manufacturers failure may occur at the dome in much more damaging way.
  - Data includes motion picture and recorded pressure pulses.
  - Funded mostly out of LDRD which is finished.





ta4769

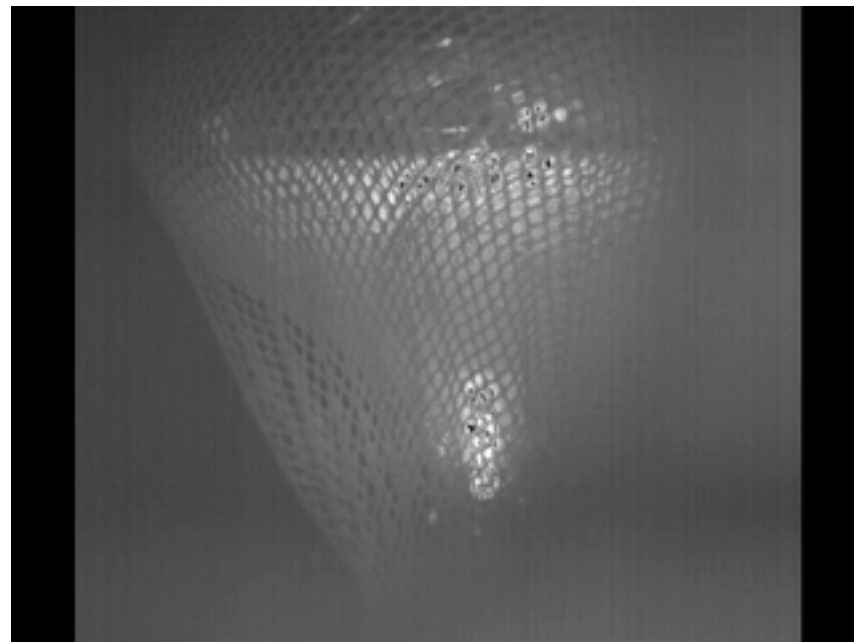
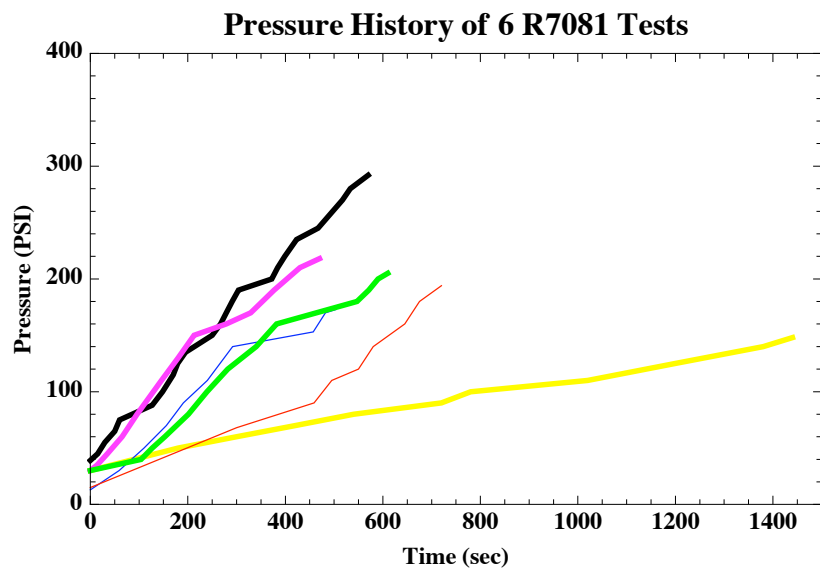




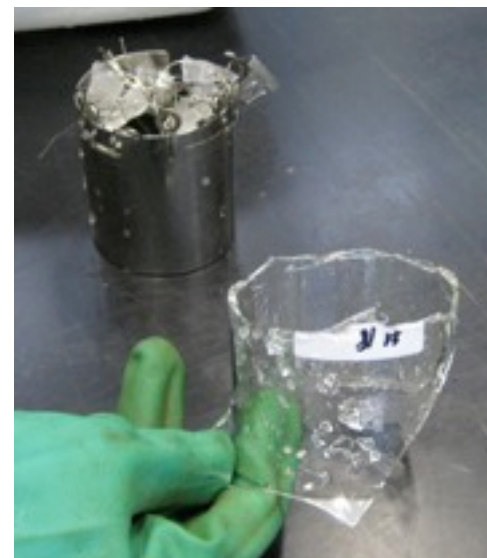
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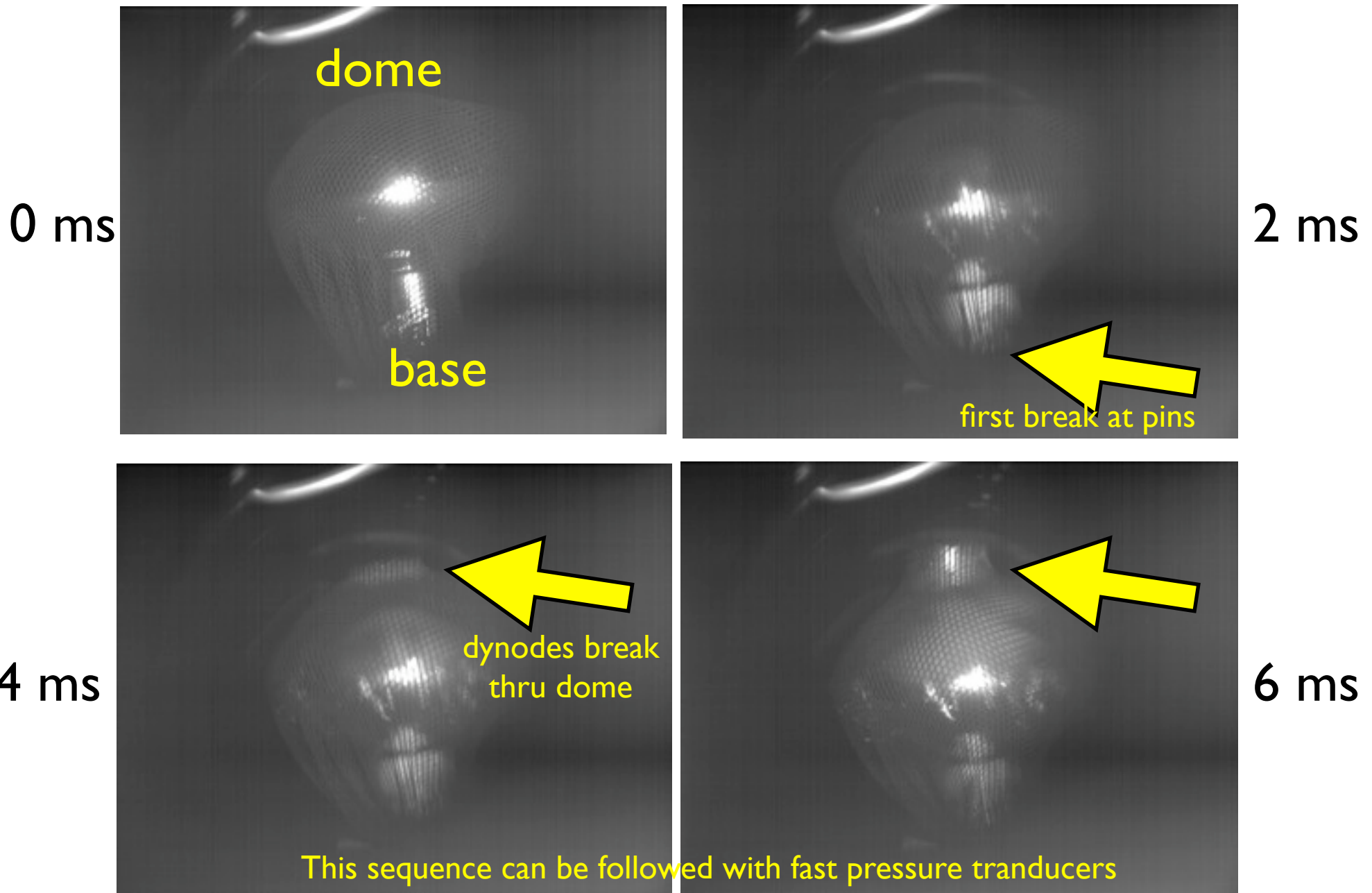




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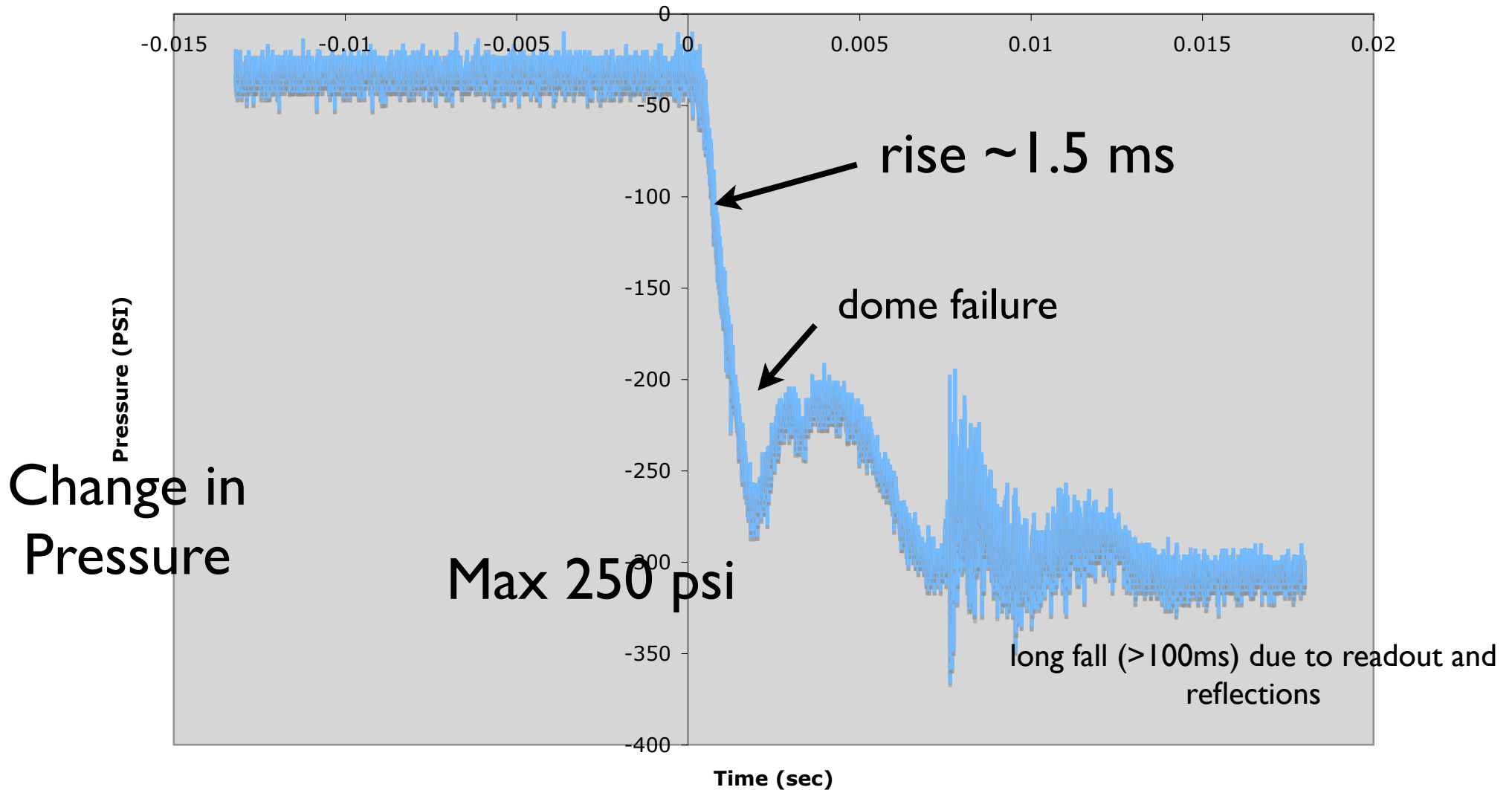
# Typical R708I failure (TA3085 failed at 13.4 bar)





# Typical R708I (ta3085 at 13.4 bar (194 psi))

## Pressure Versus Time at Implosion



sensor at 40 inch

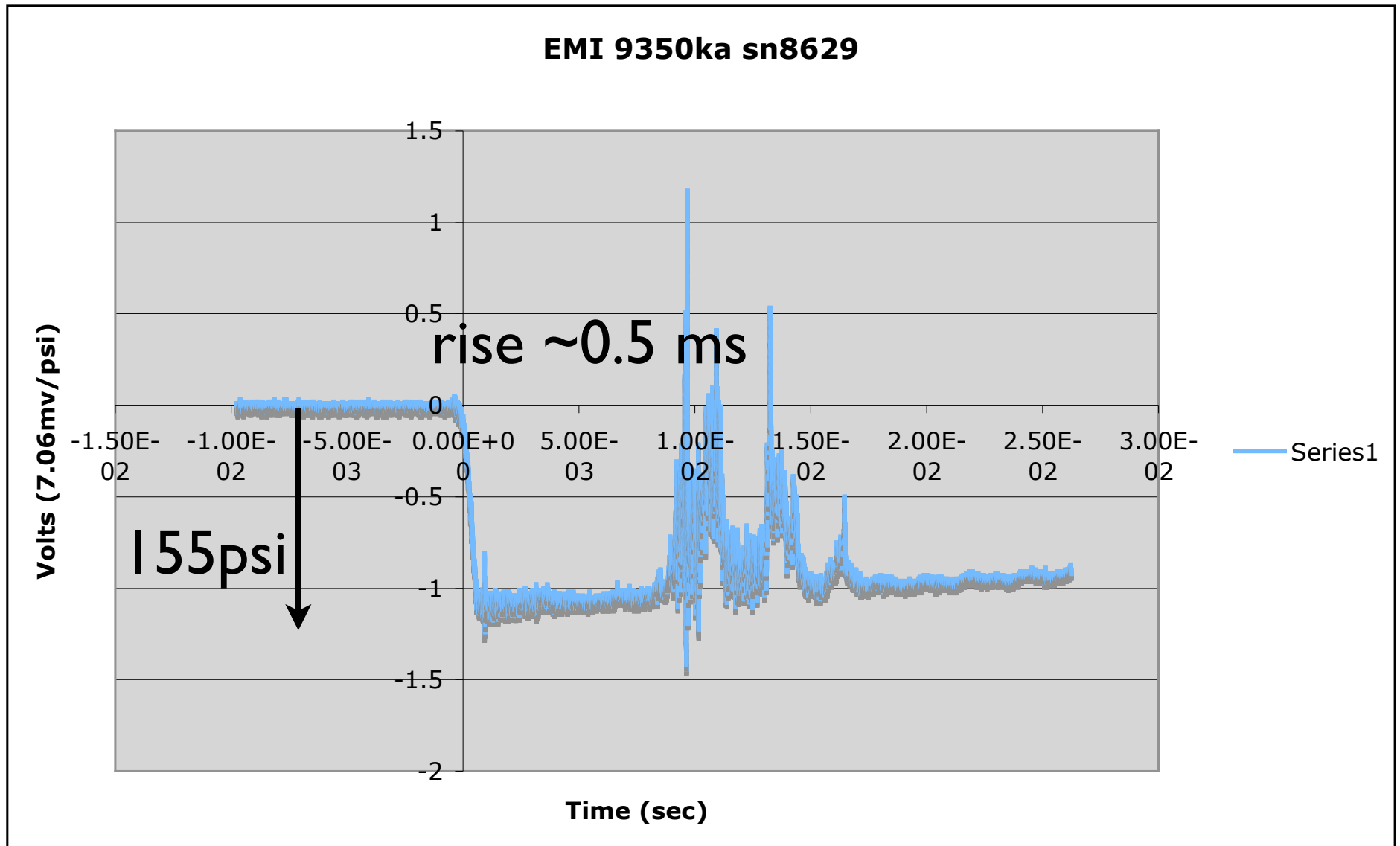
No shock wave because  
tank too small

# ETL tube #2



broke at 104 psi      sn 8629      2 microsec/frame

# Broke at 104 psi



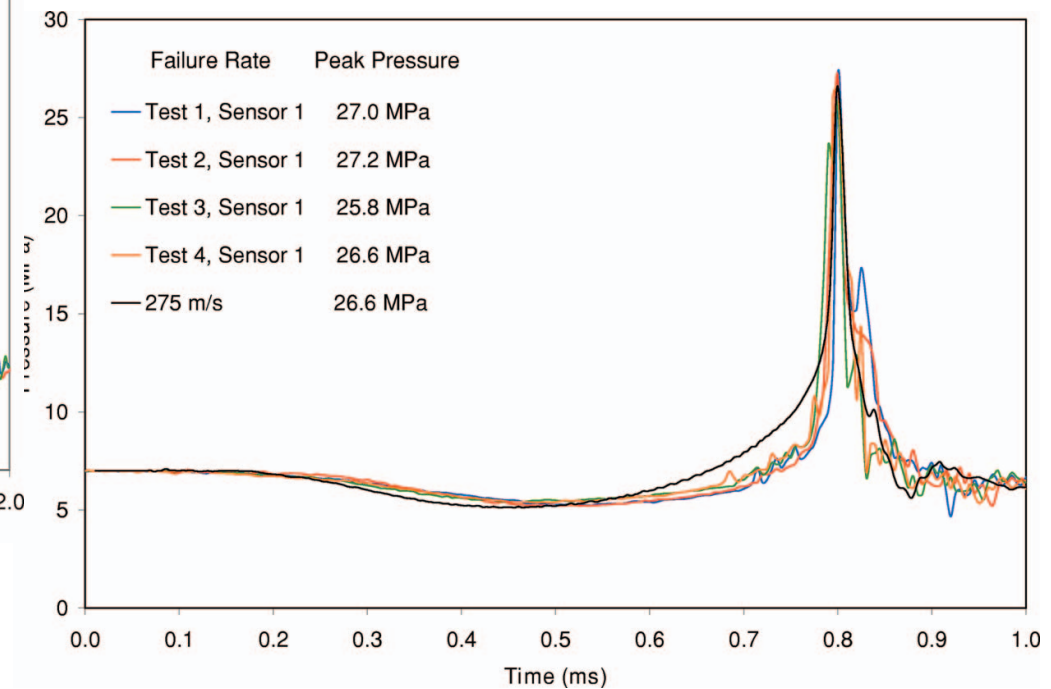
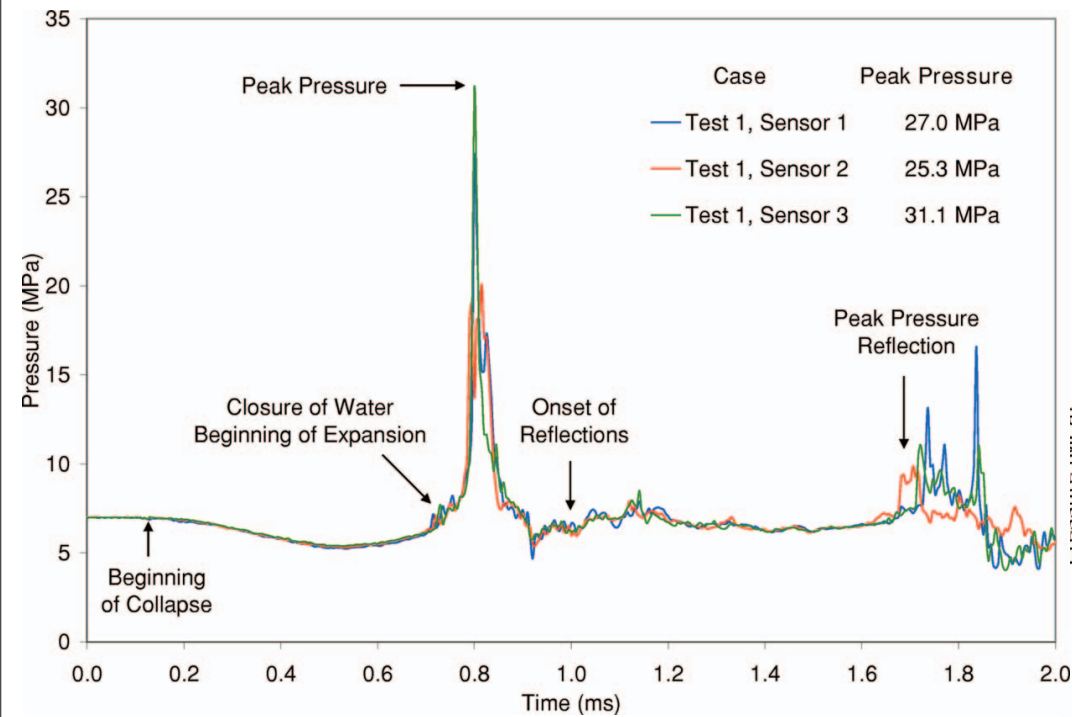
sensor at 40 inch



# Materials

- <http://nwg.phy.bnl.gov/~diwan/300kt/>
- analysis example
- J. Acoust. Soc. Am. 121 (2), Feb. 2007
- Stephen E. Turner, Underwater implosion of glass spheres, Naval Undersea Warfare Center, Newport RI.

# Simulation from paper



# Possible Team for this work

- BNL: Milind Diwan, Ken Sexton (measurements)
- BNL: Nick Simos, Steve Bellavia (Computational Fluid Dynamics).
- NUWC (Navy Undersea Warfare Center): Stephen Turner, Joseph Ambrico (DYSMAS, measurement facilities)
- CAE associates.



# Meetings

- Meeting was held with CAE associates to inform and get opinion on our work.  
6/16/2009
- Second Meeting was held on 7/13/2009 (Monday) with NUWC and CAE.

# General conclusions

- It may not be possible to model the initial pressure pulse within a factor of a few.
- Model will require benchmark tests.
- Model can be made to agree with tests by varying some parameters, but it is difficult to judge validity.
- An initial pressure pulse depends on materials. In particular, the pressure pulse depends on the speed with which the material is torn.
- Also depends on geometry of the nearby structures. i.e. water has to be available for inflow.

# Continued

- An initial evaluation assuming instantaneous failure is underway, but will overestimate the pulse by at least a factor of 2 and as much as a factor of 10.
- It is likely that with the smaller volume of R708I, there is no shock wave or minimum mitigation is needed at 6-7 bar.
- Propagation of the shock wave can be done with same code.
- Evaluation of whether a tube breaks under a static plus a dynamic load is not possible without testing.



# Capabilities

- NUWC can do the needed calculations.
- NUWC also has testing facilities.
- Testing with explosive charges is possible.
- a 10 ft diameter tank upto 100 bar exists in New Port RI.



FIG. 1. Test stand with test sample and instrumentation installed.

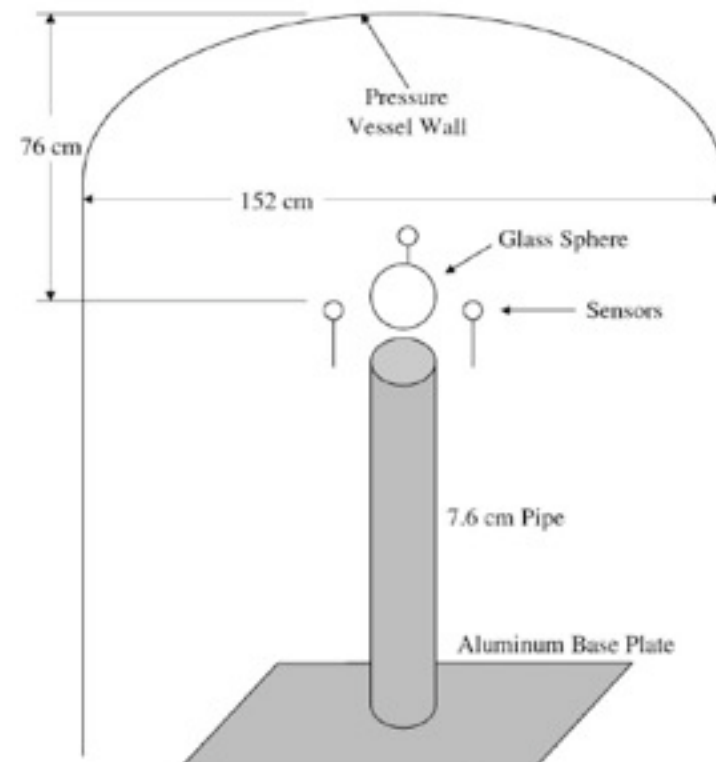


FIG. 2. Test stand schematic.

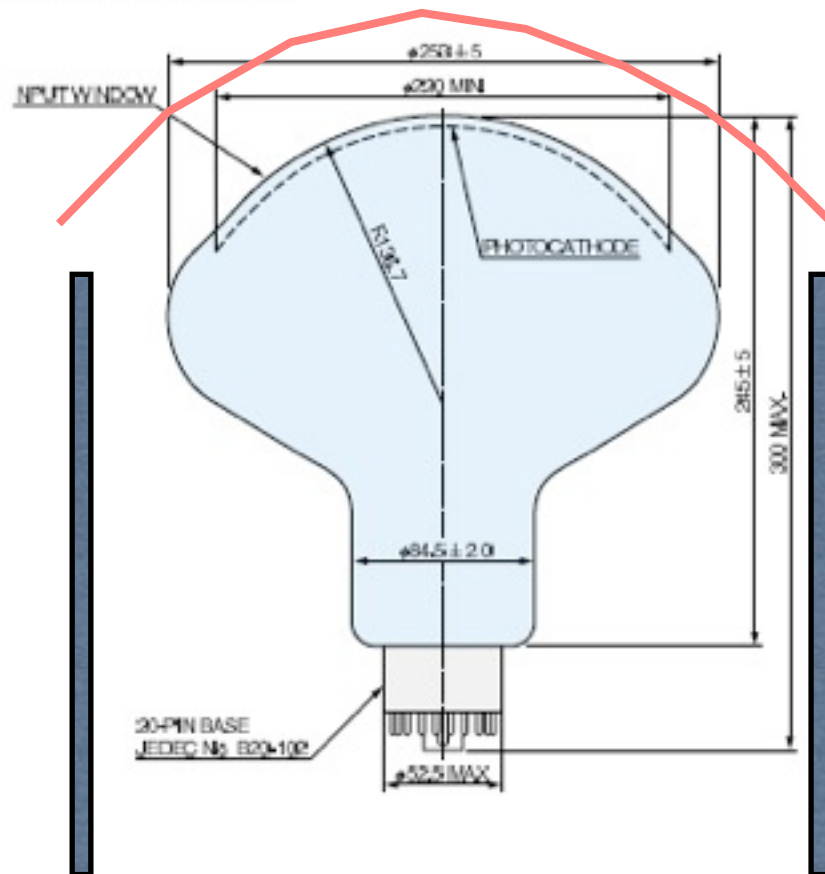
# Plan for work

- Initial calculations from NUWC.
- Start work on water proof base design to evaluate what potting does to pressure performance. No data here. Might do 2 tests.
- Perform at least one test in the NUWC tank with their instrumentation.
- Initial evaluate of 3 choices for a baffle.
- CAE/BNL will evaluate effect of baffle on pressure pulse.
- Test at NUWC with explosive charges on several tubes.

# Baffle choices

Cover if needed

●R7081, R7081-20



Cylindrical  
baffle. Material:  
acrylic,  
polypropylene,  
fabric.

evaluate with and without cover.



# Summary

- We have the intellectual and hardware resources for the pressure performance evaluation and design.
- Some issues regarding agreements with outside organizations
- There is not much engineering \$ in S4 or DOE side of the budgets for this work because it got tossed back and forth. Might need to think about this.